

Evaluation of the moments of inertia of forced split fragments for $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$ nuclei

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Abstract: This study develops an innovative theoretical framework that integrates a macroscopic liquid-drop model with microscopic superfluid theory to calculate moments of inertia for fission fragments, extending our previous spontaneous fission approach to include the neutron-induced threshold fission of $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$. The model provides a comprehensive description of fission dynamics by simultaneously accounting for collective vibrational modes (bending and wriggling) and their influence on spin distributions while systematically investigating the deformation dependence of moments of inertia. Our calculations demonstrate close agreement with experimental data, validating the model's reliability for both fundamental nuclear fission studies and practical applications in reactor physics. The unified treatment of macroscopic and microscopic effects offers new insights into fission mechanisms and enables accurate predictions of fragment characteristics across the entire mass range. These results provide a solid basis for future studies on exotic fission processes and advanced applications in nuclear energy. The methodological advances presented here create new possibilities for theoretical studies of various heavy-ion reactions and fission phenomena in superheavy nuclei.

Keywords: nuclear fission, moments of inertia, fission fragments, statistical model, microscopic model, angular momentum distribution

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I. INTRODUCTION

Modern nuclear fission studies combine experimental [1] and theoretical [2, 3] approaches to investigate the binary fission of $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$ isotopes induced by threshold-energy neutrons. This process involves the formation of a compound nucleus undergoing fission that decays into two significantly distinct fragments—light and heavy—characterized by different charges, masses, spins, and other physical parameters. The analysis of these disparities is crucial for understanding fission mechanisms as it enables establishing correlations between the parent nucleus structure, excitation energy, deformation dynamics, and final fragment characteristics.

A particularly important aspect of contemporary research involves studying quantum mechanical interference effects, which are critical for describing fundamental binary fission characteristics. An adequate theoretical description of these phenomena requires quantum ap-

proaches based on analyzing nuclear and particle wave functions at different stages of the fission process. Significant contributions to this theory have been made by both international [4] and domestic [5] researchers, whose work has shaped the modern understanding of quantum aspects in nuclear processes.

Nuclear fission represents a multistage dynamic process in which various degrees of freedom are sequentially activated, determining key fragment characteristics: spin distributions (SDs), energy spectra, and kinematic parameters. The central phenomenon in this process involves nonequilibrium deformations of the nucleus resulting from significant nonlinear deviations from equilibrium configurations. These deformations lead to accumulation of significant excitation energy (up to tens of MeV), which is subsequently redistributed within the system and determines important characteristics such as prompt neutron multiplicity and features of spin state distributions.

The terminal stage of nuclear fission is characterized by intricate energy redistribution processes and stabiliza-

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tion of resulting fragments. During this phase, the excess energy is released primarily through two channels: neutron evaporation and γ -quantum emission. These processes, governed by fundamental nuclear physics principles, reflect specific features of nucleon-nucleon interactions and angular momentum redistribution dynamics within the system. The cascade particle evaporation serves as an efficient mechanism for dissipating excitation energy, progressively transitioning fragments to minimal-energy states—either ground or weakly excited states.

The pivotal stage of the entire process culminates with the completion of cascade transitions as the fragment system attains thermodynamic equilibrium. At this juncture, the stable configurations of the fission fragments become definitively established, with their spin characteristics—both magnitude and spatial orientation—becoming fixed and remaining invariant thereafter. This phase holds fundamental significance as it precisely determines the ultimate spin states of the fragments, which subsequently govern all their physical properties and interaction modalities with surrounding nuclear and atomic systems. The complete stabilization of spin parameters signifies the conclusion of the dynamic fission phase and the system's transition to an equilibrium state.

These investigations significantly improve our understanding of the fundamental principles of nuclear fission, spanning from the initial scission of the nuclear system to the formation of final reaction products. The obtained results are paramount to advancing contemporary theories of nuclear reactions and developing more accurate predictive models, which have applications in both fundamental science and applied nuclear technologies. Of particular value is the capacity to correlate theoretical predictions with experimental data on spin characteristics, serving as a crucial validation criterion for the developed theoretical frameworks.

This study extends the authors' previously developed spontaneous fission model to describe neutron-induced fission of $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$ isotopes at threshold energies. Primary emphasis is placed on a detailed analysis of non-equilibrium fragment deformations and computation of their moments of inertia employing modern high-precision theoretical methodologies. Particular attention is given to model verification through meticulous comparison of theoretical predictions with experimental data, which will not only validate the adequacy of the developed approach but also yield novel fundamental insights into fission dynamics.

An essential component of this study involves investigating the model's predictive capability regarding fragment SDs. Such analysis unveils prospects for enhanced understanding of nuclear fission mechanisms, including secondary product formation processes and specific features of energy redistribution within the system. The ob-

tained results have significant potential for advancing nuclear reaction theory and may be applied in various domains of nuclear physics.

II. METHODS OF ESTIMATION OF MOMENTS OF INERTIA

A. A model of a "cold" fission system

This study investigates the hypothesis of a sawtooth dependence of the moments of inertia on the mass number, representing a key avenue for further elucidating the internal mechanisms governing nuclear structure and fission behaviour. Understanding these dependencies is essential for a comprehensive understanding of the physical phenomena involved in the fission process, with significant implications for theoretical nuclear physics and practical applications in fields such as nuclear energy and medicine.

The process of binary threshold fission of a compound fission system (CFS) can be described using the quantum theory of fission based on the generalised model of the nucleus proposed in [4]. This model provides a versatile and robust framework that accounts for both nucleonic and collective degrees of freedom. These interactions, associated with nuclear deformation and vibrational dynamics, enable a deeper understanding and more accurate modelling of the dynamics of the fission process. Incorporating such factors can significantly enhance the precision of predictions, particularly for the complex and multifaceted mechanisms occurring in the nucleus during the fission. This approach facilitates comprehensive modeling of critical aspects, from the nuclear deformations to vibrational effects that influence the final outcome of the process.

Forced fission occurs when a target nucleus (A, Z) captures a neutron with a kinetic energy T_n , corresponding to the threshold energy for a given parent nucleus. This process leads to excitation of the nucleus, which accumulates an excitation energy $B_n + T_n$, including both the contribution from the binding energy of the captured neutron B_n (approximately 6 MeV) and the additional kinetic energy of the neutron T_n (approximately 2 MeV). Within a timescale of $T_0 \approx 10^{-22}$ s, the excited nucleus rapidly transitions to the neutron resonance CFS state. To describe the wave function ψ_K^{JM} of this state, we use an approach based on Wigner's random matrix theory [6, 7, 8], which provides a precise framework for describing the quantum states of a CFS:

$$\psi_K^{JM} = \sum_{i \neq 0} b_i \psi_{iK}^{JM}(\beta_\lambda). \quad (1)$$

In this theoretical model, the functions ψ_{iK}^{JM} and $\psi_{0K}^{JM}(\beta_\lambda)$ represent components describing distinct aspects of the

CFS dynamics. Specifically, ψ_{iK}^{JM} is associated with i -quasiparticle excited state of the system, and $\psi_{0K}^{JM}(\beta_\lambda)$ reflects the collective deformation motion of the CFS, which is essential in the transient dividing state first introduced by Bohr [4]. The excitation energy $B_n + T_n$, associated with the state $\psi_{0K}^{JM}(\beta_\lambda)$, corresponds to the transient state of CFS, where the system takes the form corresponding to fission. The formula for the wave function in this model considers the contribution of these states through the squares of the coefficients b_i and b_0 , which are weighted averages $1/N$, where N is the total number of quasiparticle states contributing to the wave function (1), for all quasiparticle states involved in the formation of the wave function.

The forced threshold fission of a CFS occurs with significant probability if the excitation energy $B_n + T_n$ exceeds the heights of the internal B_I and external B_{II} fission deformation barriers. This process is characteristic of target nuclei ^{238}U and ^{232}Th , interacting with neutrons of threshold energies. This is supported by Fig. 1, where the upper arrow indicates the critical energy at which the fission probability significantly increases.

The parameters of forced threshold fission of CFS are described through two fundamental postulates outlined in the theoretical model [4]. The first postulate states that the axial symmetry of the CFS is preserved during the fission process. This assumption is supported by empirical data demonstrating a high degree of fission symmetry in numerous of experimental studies. The second postulate posits that the projection K of spin J of the fissioning nucleus onto the symmetry axis remains constant throughout the process, beginning from the moment when the nucleus overcomes the external saddle state of the deformation potential. This hypothesis is crucial in theoretical analyses because it enables us to reliably describe the dynamics of fission and the spin characteristics of the

system at various stages [9].

A key factor preventing the preservation of the spin projection on the symmetry axis during fission is the intense thermal excitation of both the fissile nucleus itself and the fragments formed. An increase in temperature enhances the dynamical Coriolis interaction, which, under conditions of thermal excitation, becomes dominant and significantly affects the system's behavior. According to theoretical studies [4, 10, 11], this effect leads to a statistical redistribution of all possible values of the projection K of spin J on the symmetry axis, particularly at intermediate temperatures. This redistribution significantly influences the fission dynamics, reducing the distinctions between spin orientations and complicating accurate modeling of the system's behavior at different stages.

The statistical mixing of K spin projections J near the moment of fission of a CFS into fragments can be considered a mechanism leading to a "loss of memory" about the initial values of these projections associated with transient fission states. This effect explains the absence of all types of asymmetries in the angular distributions of both binary and ternary nuclear fission products, including asymmetries related to odd and even values of spin projections [12]. A similar phenomenon is observed for asymmetries with different parities with respect to the P - and T -symmetry operators characterizing the properties of fission products, which is confirmed by experimental data [13, 14].

These experimental results indicate that the "cold" character of the system is preserved through all stages of the fission process. This holds true both for the stage of the downward motion of the nucleus from the outer saddle point of the deformation potential and for the formation of the angular distributions of fission products. Thus, the stability of the quasi-static characteristics of the system, even under conditions of low-temperature dy-

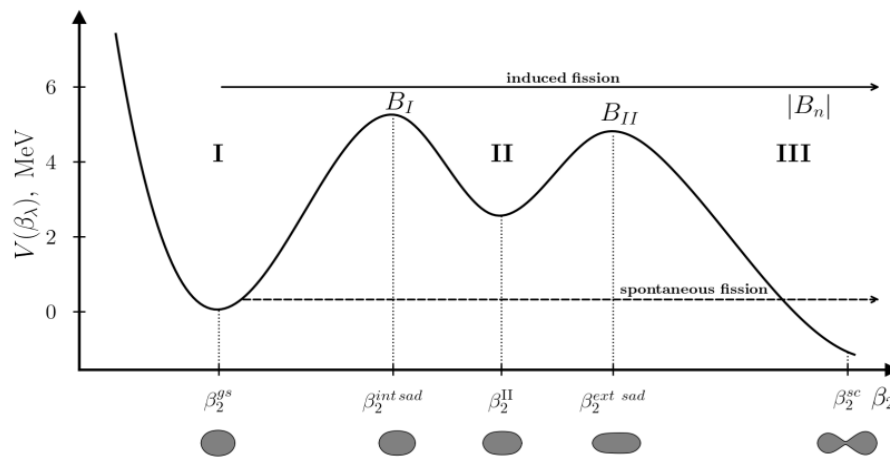


Fig. 1. Principal diagram of the potential V as a function of the quadrupole deformation of the nucleus β_2 . Region I corresponds to the ground state of the nucleus with β_2^{gs} , II to the isomeric states, and III to the out-of-barrier region where the nucleus decays into fission fragments. B_I refers to the internal barrier, and B_{II} refers to the external barrier.

namics, confirms the critical role of slow processes of angular momentum redistribution in fission.

B. Determination of nonequilibrium pre-fragment deformations

According to the postulate on the "cold" nature of a CFS discussed in the previous section, all excitation energy accumulated by pre-fragments during their formation is preferentially converted into collective deformation states. These states induce significant nonequilibrium deformations in the pre-fragments, which play a pivotal role in the subsequent fission dynamics. After the CFS rupture, the fission fragments undergo thermalization, followed by a de-excitation process accompanied by neutron emission over a characteristic timescale τ_{nuc} . This sequential transition between stages enables a quantitative assessment of the excitation levels of the fragments. Of particular significance in this context is the work of Strutinsky [15], which established the relationship between the collective deformations of fragments and their excitation energy within the framework of the liquid-drop model of the nucleus. This dependence enables us to not only characterize pre-fragments by their excited state but also determine a quantitative relationship between the degree of nonequilibrium deformation and the excitation energy, as well as the number of neutrons emitted by fragments during their thermal relaxation. These results not only deepen our understanding of the physical processes occurring during the fission stages but also lay the foundation for refining models of the energy and angular distribution of fission products.

Data on the excitation energies of the nuclei $^{238}\text{U}(n, f)$ and $^{232}\text{Th}(n, f)$, formed immediately after the fission system ruptures, are essential for quantitatively describing nonequilibrium deformations of fission fragments. An extensive analysis of literature sources provided the necessary data on excitation energies for the reaction of forced fission induced by neutrons at threshold energies, as presented in [16]. In particular, Fig. 2 shows the excitation energies of fission fragments as a function of their mass number A , which enables us to use these data for the subsequent analysis of nonequilibrium deformations.

However, despite an extensive search in the available literature, data on excitation energies for fragments produced in the forced fission of ^{238}U nuclei by neutrons at threshold energies could not be found, and only neutron yields for this nucleus have been reported in [17]. Consequently, a methodologically sound approach is required to analyze neutron yields and their relationship to excitation energies. This study focuses on applying the approaches described in [18] to analyze neutron yields, conduct an in-depth analysis and achieve a more accurate interpretation of the results. Two theoretical approaches from [18] are considered: the first employs the FREYA software package [19], and the second is based on a the-

oretical analysis of fission fragment decay, incorporating strict conservation of total angular momentum and parity, as proposed in [20]. Both approaches, when applied to the spontaneous fission of ^{252}Cf , showed only qualitative agreement but lacked reasonable quantitative agreement, prompting the use experimental data from [21]. In this study, we directly utilize neutron yields from [17] presented in Fig. 3 for a forced fission induced by neutrons at threshold energies for the nucleus $^{238}\text{U}(n, f)$.

Having determined the neutron yields, we proceed to calculate the excitation energy U . Several approaches exist, each based on different theoretical assumptions and empirical data. One such method, proposed about a

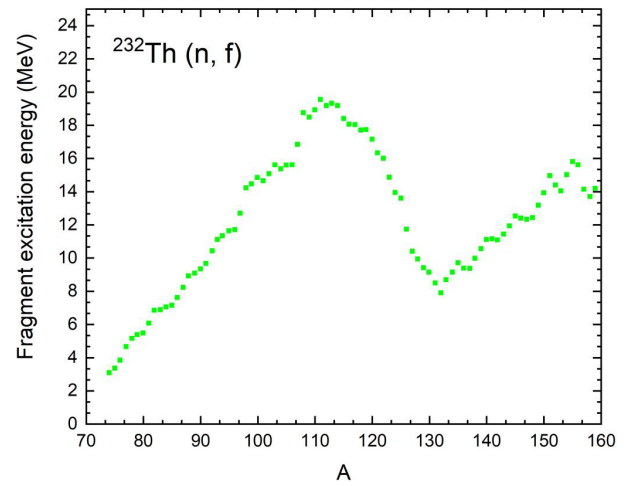


Fig. 2. (color online) Dependence of the average excitation energies on the mass of fragments produced during forced threshold fission of $^{232}\text{Th}(n, f)$ by neutrons with a kinetic energy of 2 MeV [16].

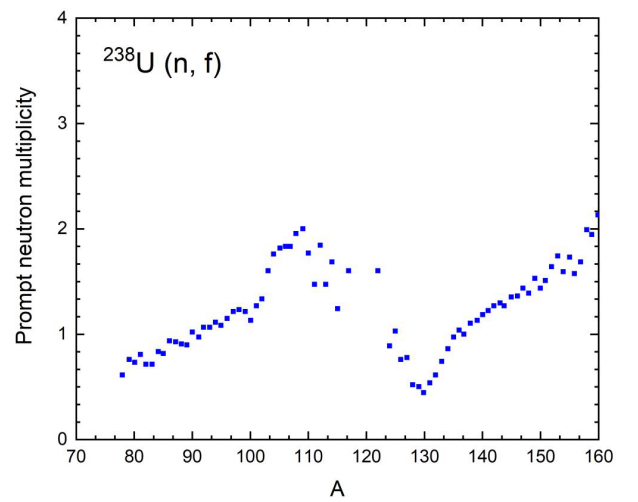


Fig. 3. (color online) Dependence of the average neutron multiplicity on the mass of fragments produced during forced threshold fission of $^{238}\text{U}(n, f)$ by neutrons with a kinetic energy of 2 MeV [17].

quarter of a century ago [20], provides a conceptual framework that establishes a quantitative relationship between U and the neutron yield multiplicity. Within this methodology, this relationship is expressed as follows:

$$U = 5 + 4\nu + \nu^2, \quad (2)$$

where ν represents the neutron multiplicity.

Another advanced method, based on theoretical developments presented in [22], offers an improved model for calculating U . This approach extends the existing conceptual framework by incorporating more complex interaction mechanisms and relationships between key physical parameters that determine the dynamics of the fission process. The methodology includes a detailed consideration of collective and single-quasiparticle degrees of freedom, as well as the influence of different deformation configurations on the excitation energy. Consequently, a mathematical dependence is formalised, expressed by

$$U = 7(\nu + 3/7), \quad (3)$$

The linear dependence indicates that, as the neutron multiplicity increases, the average excitation energy also increases. This phenomenon occurs because the residual nucleus approaches a state near the stability line.

Using Eq. (2), we calculated the average excitation energy U for the nucleus $^{238}\text{U}(n, f)$, as shown in Fig. 4 by the solid green line. In parallel, applying Eq. (3), the averaged value of U , which is represented in Fig. 4 by the yellow line, is calculated.

The comparative analysis, presented in Fig. 4, demonstrates a high degree of agreement between the two meth-

ods based on Eqs. (2) and (3) across the entire parameter range considered. Both approaches preserve the characteristic sawtooth structure observed in the distribution of neutron multiplicity and the excitation energy behavior of fragments. This structure reflects the complex dynamics of energy redistribution between collective and single-quasiparticle degrees of freedom at different fission stages. Thus, these results confirm the effectiveness of the proposed methods in describing the thermodynamic characteristics of the fission process and their reliability in modeling the dynamic behavior of fission systems.

The next stage of the analysis focuses on establishing the relationship between the excitation energy of fission fragments and their nonequilibrium deformations at the pre-fragmentation stage. To address this, we apply the method proposed by Strutinsky [15], which utilizes the Nilsson level scheme to calculate shell corrections incorporated into the liquid drop model (LDM) for a more accurate estimation of the total excitation energy.

Strutinsky's corrections depend not only on the number of occupied quantum levels but also on nuclear deformation, enabling a significant improvement in the accuracy of accounting for nuclear degrees of freedom in the total excitation energy. This is particularly critical for analyzing the dynamics of nonequilibrium processes occurring at the pre-fragment formation stage in fission reactions.

In the framework of the considered approach, we assume that the total U can be represented through the strain energy calculated within the LDM. This energy is divided into two key components: surface and Coulomb energies. Both of these components can be described using simplified analytical forms, which are defined by Eq. (4):

$$U = \sigma A^{2/3} (0.4(1-x)\alpha^2 - 0.0381(1-2x)\alpha^3), \quad (4)$$

where $\sigma = 16$ MeV, $x = Z^2/(45A)$, and α is the deformation parameter defined by the relation $\alpha = 2\beta/3$.

Using expression (4), we can calculate the equilibrium strain energy by substituting the equilibrium strain values obtained from [23]. Because the results obtained using Eqs. (2) and (3) are consistent with each other to a sufficiently high degree for the entire fission fragmentation region, any of the above formulae can be used in the present study. By adding the excitation energy calculated using either formulae to the equilibrium strain energy, we obtain the nonequilibrium excitation energy.

From the nonequilibrium deformation energy, Eq. (4) is applied to solve the inverse problem, determining the nonequilibrium deformations of fission pre-fragments. All calculated values are presented in Tables 1 ($^{232}\text{Th}(n, f)$) and 2 ($^{238}\text{U}(n, f)$).

The structure of Tables 1 and 2 is arranged in a sys-

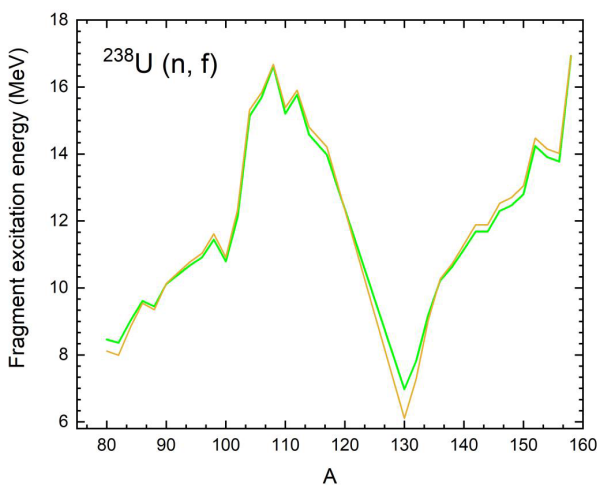


Fig. 4. (color online) Dependence of the average excitation energy on fragment mass in the fission of $^{238}\text{U}(n, f)$ by neutrons at threshold energies, calculated using Eq. (2) (solid green line) and Eq. (3) (yellow line).

Table 1. Quadrupole deformation parameters; moments of inertia (normalized to rigid-body values) for oscillator, rectangular well, and hydrodynamic models; and resulting fragment spins for $^{232}\text{U}(n,f)$.

Nucleus		I_{osc}/I_o	I_{rec}/I_o	I_{hyd}/I_o	$I_{b(\text{osc})}; I_{b(\text{rec})}; I_{b(\text{hyd})}$	$I_{w(\text{osc})}; I_{w(\text{rec})}; I_{w(\text{hyd})}$	J_{osc}	J_{rec}	J_{hyd}	
d=3.5	^{82}Ge	0.392	0.639	0.252	0.114	62.09	76.95	5.54	4.70	4.05
						34.39	40.25			
						19.63	22.28			
d=4.2	^{151}Ce	0.654	0.854	0.473	0.270	57.71	74.57	8.35	7.39	6.52
						29.77	37.60			
						17.26	20.42			
d=4.1	^{84}Ge	0.418	0.688	0.320	0.129	56.22	70.77	5.46	4.59	3.92
						27.76	33.34			
						16.27	19.38			
d=3.4	^{149}Ba	0.599	0.812	0.401	0.235	53.04	70.99	7.82	6.69	5.88
						25.18	33.51			
						14.56	18.13			
d=4.4	^{86}Se	0.437	0.699	0.324	0.139	59.83	79.66	6.10	5.05	4.30
						33.07	42.17			
						21.72	26.19			
d=2.9	^{145}Ba	0.716	0.854	0.472	0.310	52.15	71.80	8.52	7.48	6.91
						25.10	34.06			
						13.33	17.67			
d=2.85	^{88}Kr	0.474	0.724	0.330	0.160	49.21	69.71	6.79	5.62	4.75
						22.36	31.30			
						11.87	16.79			
d=2.6	^{143}Xe	0.526	0.788	0.358	0.190	48.78	70.79	9.09	7.50	6.37
						22.56	32.09			
						11.59	17.17			
d=2.05	^{141}Xe	0.525	0.800	0.370	0.190	47.55	70.74	9.58	7.97	6.63
						21.99	32.03			
						11.11	17.55			
d=3.3	^{139}Xe	0.521	0.800	0.370	0.187	47.63	71.08	11.01	9.16	7.48
						22.59	33.71			
						10.01	15.55			
d=3.1	^{141}Te	0.487	0.795	0.377	0.167	47.48	71.37	7.54	6.25	5.02
						22.86	34.13			
						10.37	16.55			
d=2.6	^{139}Te	0.502	0.806	0.388	0.176	44.42	71.89	8.14	6.80	5.44
						20.42	33.72			
						7.70	16.80			
d=2.6	^{96}Sr	0.649	0.806	0.390	0.267	20.42	33.72	7.30	6.07	5.55
						7.70	16.80			
d=2.6	^{137}Te	0.436	0.796	0.366	0.138	44.42	71.89	8.84	7.23	5.15
						20.42	33.72			

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Table 1-continued from previous page											
Nucleus		I_{osc}/I_o	I_{rec}/I_o	I_{hyd}/I_o	$I_{b(osc)}; I_{b(rec)}; I_{b(hyd)}$		$I_{w(osc)}; I_{w(rec)}; I_{w(hyd)}$		J_{osc}	J_{rec}	J_{hyd}
d=2.7	^{98}Sr	0.719	0.869	0.488	0.312	43.91	75.65				
						20.31	38.13	7.72	6.69	6.10	
						8.12	19.52				
d=2.55	^{135}Te	0.454	0.800	0.370	0.148			8.87	7.09	5.20	
						38.35	67.44				
						18.57	32.54	7.79	6.49	6.41	
d=2.9	^{98}Zr	0.731	0.792	0.380	0.320	7.57	19.33				
								8.80	7.36	5.19	
						38.36	70.87				
d=2.9	^{100}Zr	0.735	0.854	0.454	0.323	19.71	37.00	7.46	6.37	6.03	
						7.57	19.86				
								8.03	6.76	4.79	
d=3.9	^{133}Sn	0.443	0.720	0.370	0.142	29.48	66.14				
						11.63	33.36	5.25	3.89	3.25	
						6.32	20.47				
d=3.9	^{130}Sn	0.411	0.583	0.230	0.125			5.80	5.21	4.74	
						19.66	53.24				
						7.85	25.70	5.49	4.18	3.64	
d=3.7	^{103}Zr	0.774	0.899	0.533	0.347	4.97	18.41				
								7.02	6.11	5.76	
						34.76	69.53				
d=4.1	^{132}Te	0.371	0.682	0.264	0.104	13.45	33.17	6.23	4.62	3.40	
						5.30	17.95				
								6.23	5.48	5.05	
d=4.6	^{101}Sr	0.740	0.896	0.508	0.326	31.98	66.07				
						12.65	31.97	5.47	4.10	3.46	
						6.94	18.80				
d=4.6	^{99}Sr	0.727	0.914	0.518	0.318			5.62	4.94	4.40	
						40.57	70.29				
d=3.2	^{136}Te	0.430	0.738	0.320	0.135	17.59	33.26	8.08	6.36	4.78	
						7.42	17.53				
								7.11	6.05	5.49	
d=3.4	^{97}Sr	0.680	0.844	0.445	0.287	42.10	70.40				
						18.29	33.73	7.53	5.90	4.75	
						8.49	16.87				
d=3.4	^{138}Te	0.455	0.739	0.321	0.149			6.44	5.51	4.73	
						42.33	68.36				
d=3.8	^{138}Xe	0.473	0.737	0.319	0.159	18.32	30.53	7.01	5.62	4.51	
						9.13	17.40				
								5.83	4.80	4.33	
d=2.2	^{95}Kr	0.623	0.787	0.369	0.250	44.94	69.03				
								11.12	8.95	7.72	
						19.62	30.94				
d=2.2	^{140}Xe	0.516	0.749	0.327	0.184	11.04	17.58				
								8.75	7.21	6.28	
						47.02	69.83				
d=2.2	^{142}Xe	0.517	0.765	0.335	0.185	20.59	30.83	10.90	8.84	7.67	
						11.37	16.72				
								8.36	6.83	5.83	
d=2.2	^{91}Kr	0.514	0.780	0.350	0.183						

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Table 1-continued from previous page										
Nucleus		I_{osc}/I_o	I_{rec}/I_o	I_{hyd}/I_o	$I_{b(osc)}; I_{b(rec)}; I_{b(hyd)}$		$I_{w(osc)}; I_{w(rec)}; I_{w(hyd)}$	J_{osc}	J_{rec}	J_{hyd}
d=3.3	¹⁴² Ba	0.535	0.754	0.344	0.196	46.74	68.95	8.13	6.59	5.88
						21.32	32.57			
						12.15	17.37			
d=2.7	⁹¹ Se	0.507	0.762	0.386	0.179			6.26	5.23	4.40
						49.84	71.25			
						23.48	33.65			
d=3.0	¹⁴⁴ Ba	0.558	0.777	0.366	0.210	13.47	18.18	10.02	8.29	7.40
						50.77	70.98			
d=3.0	¹⁴⁶ Ba	0.565	0.771	0.353	0.214	23.25	32.08	9.37	7.75	7.05
						14.09	18.09			
d=3.0	⁸⁷ Se	0.459	0.764	0.334	0.151			6.88	5.62	4.82
						52.73	79.08			
						24.25	33.46			
d=3.0	¹⁴⁸ Ce	0.594	0.772	0.355	0.232	15.85	19.32	9.85	8.08	7.67
d=2.9	⁸⁵ Ge	0.435	0.769	0.366	0.138	59.99	77.99	7.08	5.86	5.02
d=2.9	¹⁵⁰ Ce	0.640	0.840	0.448	0.261	31.99	39.87	11.22	9.77	7.80
						18.64	21.71			
	⁸³ Ge	0.640	0.750	0.328	0.128			7.67	6.45	5.52

Table 2. Quadrupole deformation parameters; moments of inertia (normalized to rigid-body values) for oscillator, rectangular well, and hydrodynamic models; and resulting fragment spins for ²³⁸U(*n*,*f*).

Nucleus		I_{osc}/I_o	I_{rec}/I_o	I_{hyd}/I_o	$I_{b(osc)}; I_{b(rec)}; I_{b(hyd)}$		$I_{w(osc)}; I_{w(rec)}; I_{w(hyd)}$	J_{osc}	J_{rec}	J_{hyd}
d=4.7	^{82}Ge	0.372	0.599	0.232	0.105	72.80	86.61	5.92	5.12	4.46
						43.10	48.45			
						25.28	27.07			
d=4.5	^{157}Nd	0.723	0.907	0.537	0.315			9.15	8.24	7.30
						62.13	80.50			
						31.40	38.96			
d=4.5	^{84}Se	0.516	0.717	0.295	0.184	18.69	23.40	5.43	4.50	3.97
d=4.1	^{155}Ce	0.622	0.831	0.420	0.250	64.14	84.65	7.85	6.74	5.90
						34.24	44.04			
						22.90	28.02			
d=4.1	^{86}Se	0.527	0.766	0.366	0.191	63.27	84.39	9.41	8.13	7.52
						35.07	45.02			
						21.76	27.26			
d=4.1	^{153}Ce	0.702	0.843	0.450	0.301			6.37	5.41	4.76
d=4.1	^{88}Se	0.536	0.756	0.356	0.197			9.15	8.03	7.20
d=4.3	^{151}Ce	0.690	0.855	0.474	0.294	61.41	82.89	5.96	5.03	4.40
						32.86	43.07			
						20.15	25.67			
d=4.3	^{88}Kr	0.533	0.770	0.366	0.194			8.41	7.29	6.54
d=3.9	^{151}Ba	0.663	0.841	0.450	0.276	58.76	81.42	6.45	5.39	4.79
						29.45	40.25			
						19.54	25.73			
d=3.9	^{90}Kr	0.561	0.772	0.368	0.211			8.97	7.59	6.96
	^{149}Ba	0.660	0.824	0.413	0.274					

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Table 2-continued from previous page

Nucleus		I_{osc}/I_o	I_{rec}/I_o	I_{hyd}/I_o	$I_{b(\text{osc})}; I_{b(\text{rec})}; I_{b(\text{hyd})}$	$I_{w(\text{osc})}; I_{w(\text{rec})}; I_{w(\text{hyd})}$	J_{osc}	J_{rec}	J_{hyd}	
d=3.5	⁹² Kr	0.602	0.783	0.371	0.237	56.76	81.06	6.94	5.78	5.19
						28.24	39.76			
						18.53	25.88			
d=3.5	¹⁴⁷ Ba	0.650	0.818	0.407	0.267			9.46	8.00	7.22
						57.01	82.61			
						31.07	43.21			
d=3.5	⁹⁴ Kr	0.632	0.784	0.372	0.256	17.52	25.88	6.97	5.86	5.24
d=3.5	¹⁴⁵ Ba	0.637	0.846	0.461	0.260			9.40	8.22	6.94
d=3.7	⁹⁴ Sr	0.627	0.811	0.407	0.253	53.44	79.86	6.40	5.38	4.74
						26.39	39.65			
						15.01	23.25			
d=3.45	¹⁴⁵ Xe	0.588	0.812	0.401	0.228			8.33	6.97	5.97
d=3.45	⁹⁶ Sr	0.659	0.816	0.416	0.273	53.02	80.97	6.78	5.72	5.11
						26.96	41.21			
						14.96	24.32			
d=2.8	¹⁴³ Xe	0.594	0.822	0.418	0.232			8.70	7.34	6.18
d=2.8	⁹⁸ Sr	0.676	0.861	0.480	0.284	51.61	82.40	8.14	7.01	6.14
						26.25	43.41			
						14.32	24.47			
d=2.9	¹⁴¹ Xe	0.587	0.822	0.418	0.228			10.09	8.40	7.12
d=2.9	⁹⁸ Zr	0.688	0.770	0.366	0.292	51.40	79.09	7.70	6.42	5.98
						26.38	39.55			
						13.22	23.72			
d=2.9	¹⁴¹ Te	0.563	0.828	0.425	0.213			9.88	8.45	6.62
d=2.9	¹⁰⁰ Zr	0.686	0.830	0.436	0.291	49.40	80.24	7.85	6.68	6.03
						24.58	40.78			
						12.56	23.37			
d=3.0	¹³⁹ Te	0.555	0.818	0.407	0.208			9.55	7.96	6.44
d=3.0	¹⁰² Zr	0.717	0.842	0.449	0.311	48.84	81.67	7.86	6.71	6.16
						25.36	42.87			
						11.86	23.99			
d=3.5	¹³⁷ Te	0.546	0.832	0.432	0.202			9.31	7.87	6.09
d=3.5	¹⁰⁴ Zr	0.754	0.849	0.462	0.334	47.75	82.59	7.16	6.14	5.75
						25.01	43.97			
						10.91	24.62			
d=2.0	¹³⁵ Te	0.530	0.840	0.440	0.192			8.20	6.93	5.17
d=2.0	¹⁰² Mo	0.712	0.797	0.384	0.308	45.54	76.54	9.73	8.11	7.74
						23.77	38.71			
						12.06	24.04			
d=3.1	¹³³ Sn	0.551	0.774	0.404	0.205			11.56	9.95	7.77
d=3.1	¹⁰⁴ Mo	0.776	0.841	0.447	0.349	31.31	66.20	7.99	6.95	6.51
						12.22	30.77			
						10.14	24.62			
d=5.0	¹³¹ Sn	0.510	0.556	0.217	0.180			7.59	5.69	5.48
d=5.0	¹³⁰ Sn	0.452	0.620	0.250	0.147	31.93	69.81	5.44	4.01	3.51
						12.87	37.95			
						7.57	22.55			
	¹⁰⁹ Mo	0.758	0.852	0.464	0.337			5.86	5.42	4.77

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Table 2-continued from previous page										
Nucleus			I_{osc}/I_o	I_{rec}/I_o	I_{hyd}/I_o	$I_{b(osc)}; I_{b(rec)}; I_{b(hyd)}$	$I_{w(osc)}; I_{w(rec)}; I_{w(hyd)}$	J_{osc}	J_{rec}	J_{hyd}
d=4.9	¹³² Sn	0.470	0.535	0.207	0.157	28.49	65.06	5.34	3.99	3.75
						11.02	30.99			
						8.36	22.73			
d=4.7	¹⁰⁷ Mo	0.754	0.850	0.464	0.334	40.36	76.47	5.96	5.21	4.79
						21.29	41.00			
						9.76	24.96			
d=4.8	¹³⁴ Sn	0.503	0.728	0.384	0.176	41.33	79.33	6.61	5.60	4.23
						18.03	40.56			
						8.96	22.90			
d=4.8	¹⁰³ Zr	0.741	0.889	0.527	0.326	39.60	74.76	5.77	5.10	4.57
						16.28	34.98			
						10.52	24.55			
d=3.4	¹³⁴ Te	0.522	0.708	0.291	0.188	46.23	79.75	5.98	5.13	4.81
						22.28	40.14			
						11.31	24.14			
d=3.7	⁹⁹ Zr	0.733	0.839	0.447	0.321	47.23	80.58	7.83	6.68	6.21
						22.60	41.15			
						11.87	23.33			
d=3.8	¹³⁸ Te	0.543	0.796	0.381	0.200	47.60	80.32	7.15	6.16	5.48
						22.72	41.09			
						12.83	23.60			
d=3.8	¹⁰¹ Sr	0.679	0.869	0.488	0.286	48.47	80.01	8.15	6.60	5.69
						22.72	40.39			
						13.87	24.06			
d=2.8	⁹⁹ Sr	0.672	0.869	0.487	0.281	50.91	81.48	8.66	7.48	6.52
						24.72	41.90			
						14.72	24.57			
d=2.9	¹⁴² Xe	0.593	0.799	0.388	0.231	51.15	79.53	8.46	7.30	3.56
						24.35	38.19			
						15.85	25.11			
d=3.4	⁹⁷ Kr	0.649	0.818	0.399	0.267	47.64	74.08	7.50	6.26	5.66
						25.57	38.31			
						16.39	25.05			
d=3.0	¹⁴⁴ Ba	0.620	0.721	0.387	0.248	53.75	78.76	8.03	6.74	6.10
						25.69	37.61			
						16.77	24.03			
d=3.2	¹⁴⁶ Ba	0.620	0.795	0.380	0.248	53.75	78.76	7.53	6.25	5.56
						25.69	37.61			
						16.77	24.03			
d=3.2	⁹³ Kr	0.592	0.795	0.379	0.231	53.75	78.76	7.53	6.25	5.56
						25.69	37.61			
						16.77	24.03			

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Table 2-continued from previous page

	Nucleus	I_{osc}/I_0	I_{rec}/I_0	I_{hyd}/I_0	$I_{b(osc)}; I_{b(rec)}; I_{b(hyd)}$	$I_{w(osc)}; I_{w(rec)}; I_{w(hyd)}$	J_{osc}	J_{rec}	J_{hyd}
d=4.3	^{148}Ba	0.659	0.785	0.370	0.248	55.33	79.88		
						26.08	38.20	8.10	6.67
						17.48	24.21		6.18
d=4.0	^{91}Kr	0.580	0.814	0.402	0.223			6.06	5.06
						56.54	80.40		4.45
						26.99	39.29	8.97	7.38
d=3.1	^{148}Ce	0.680	0.794	0.379	0.287	20.44	26.92		7.19
								6.58	5.54
						61.44	84.61		4.93
d=3.1	^{150}Ce	0.684	0.842	0.449	0.289	32.76	44.67	11.52	9.89
						21.09	27.00		9.11
								8.13	6.91
	^{89}Se	0.552	0.808	0.415	0.206				6.02

tematic manner. Column 1 lists the fitting parameter d defined in Eq. (6), whereas Column 2 specifies the corresponding fission fragment pairs. Column 3 presents the quadrupole deformation parameters of the fragments. Columns 4–6 present the ratios of moments of inertia calculated within the oscillator and rectangular well potentials of the superfluid model, as well as the classical hydrodynamic model, normalized to the rigid-body moment of inertia for comparative analysis of pairing quantum effects. Columns 7–8 contain the effective moments of inertia for bending and wriggling vibrations derived from all three nuclear models, whereas Columns 9–11 present the predicted fragment spins calculated on the basis of these models. This arrangement ensures direct comparison between the theoretical approaches while preserving correspondence with experimental observables, in particular for the ^{252}Cf fission system under study. The tabulated data clearly demonstrate how variations in the calculated moment-of-inertia ratios manifest in model-dependent SDs, with special emphasis on the sensitivity of the wriggling mode contribution, which had not been explicitly considered in earlier works of this type.

C. Finding the optimal model

In this study, calculations of the moments of inertia of fission fragments for the nuclei $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$ were performed based on the values of nonequilibrium quadrupole strains presented in Tables 1 and 2. These calculations employed the methodology proposed in [18], which combines hydrodynamic [24] and superfluid models, incorporating oscillatory and rectangular potentials. This approach enables more comprehensive and accurate modeling of the dynamics of nuclear fission processes, providing a detailed description of various fission stages. The resulting values of the nonequilibrium moments of inertia are presented in Tables 1 and 2, offering important information for further analyses of the dynamical as-

pects of nuclear fission.

However, direct experimental data for verifying the theoretical models are lacking; therefore, indirect methods are used to validate the calculations. The study uses the approach proposed in [18], which involves comparing the theoretical values of the mean spins of fission fragments with the experimental data published in [1], obtained for forced threshold fission of $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$ nuclei. This method provides an additional validation of the theoretical models' accuracy by comparing them with experimentally measured values, serving as an important step in refining the models and enhancing their predictive capabilities.

To perform the calculations, this study utilizes a formalism developed in recent studies [25]. Because fission fragments emerging from the CFS reach the region near the scission point exclusively in cold nonequilibrium states [11], the calculation of their mean spin values is conducted based on zero-point oscillatory wave functions in the momentum representation, as part of a more general approach [9, 25].

$$\Psi(J_{k_x}, J_{k_y}) \equiv \Psi(J_{k_x})\Psi(J_{k_y}) = \frac{1}{\pi I_k \hbar \omega_k} \exp \left[-\frac{J_{k_x}^2 + J_{k_y}^2}{I_k \hbar \omega_k} \right], \quad (5)$$

where the index k denotes the type of oscillations, bending (b) or wriggling (w), and the energies and moments of inertia of the specified zero oscillations are $\hbar \omega_w$ and I_w and $\hbar \omega_b$ and I_b , respectively. Determining the moments of inertia corresponding to transverse bending and wriggling oscillations for each particular pair of primary fission fragment (PFF) pre-delimitation formations is a challenging theoretical problem. In particular, for wriggling oscillations, the moment of inertia I_w , as demonstrated in [26, 27], can be calculated using the following formula:

$$I_w = \frac{(I_1 + I_2)I_0}{I}, \quad (6)$$

where I_1 (I_2) is the moment of inertia of each fragment, $I_0 = \frac{M_1 M_2}{(M_1 + M_2)} (R_1 + R_2 + d)^2$ is the moment of inertia of the fission core, and d – is a fitting parameter representing the distance between the ends of the fission pre-fragments; the short-range character of nuclear forces causes even small distance variations (0.5–1 fm) to dramatically alter the stiffness of both bending and wriggling vibrations, resulting in a two-fold change in spin values. Because the parameter "d" strongly affects the nuclear component of the compound nucleus potential, its variation requires careful optimization. For all three models considered, we have determined the optimal "d"-value that provides the best agreement with experimental spin data; $I = I_0 + I_1 + I_2$ is the total moment of inertia.

Moments of inertia in the solid state model can be represented by $I_{1,2} \equiv I_{i,\text{rigid}} = \frac{M_i}{5} \sum R_i^2$, where M_i is the mass of each fission fragment, $R_i = r_0 A^{1/3} [1 - \beta_i^2/4\pi + \beta_i \sqrt{5/4\pi}]$, and β_i is the quadrupole deformation parameter, with $I_{1,2}$ determined within the framework of the superfluid Migdal nucleus model [28] and differing significantly from their rigid-body counterparts $I_i = (0.4 - 0.7)I_{\text{rigid}}$, particularly for fragments near "magic" nuclei, where $I_i = (0.2 - 0.3)I_{\text{rigid}}$.

In this study, the formula proposed in [29] is applied for the moment of inertia I_b :

$$I_b = \mu R^2 I_H / (\mu R^2 + I_H). \quad (7)$$

where $\mu = M_1 M_2 / (M_1 + M_2)$ is the reduced mass, and I_H is the moment of inertia of the heavy fragment.

Using this form of SDs and performing several simple transformations, we can obtain expressions for calculating the mean PFF spins:

$$\bar{J}_i = \int_0^\infty P(J_i) J_i dJ_i = \int_0^\infty \frac{2J_i^2}{d_i} \exp\left[-\frac{J_i^2}{d_i}\right] dJ_i = \frac{1}{2} \sqrt{\pi d_i}. \quad (8)$$

where $d_i = \frac{I_i^2 I_w \hbar \omega_w}{(I_1 + I_2)^2} + I_b \hbar \omega_b$, and $i=(1,2)$ indexes the corresponding fragment. Subsequently, using Eq. (8), we obtain estimates of spins for three different models of moments of inertia, as presented in Figs. 5 and 6 for the nuclei $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$, respectively.

A comparative analysis of the theoretical curves with the experimental data presented in [1] shows reasonable agreement for both nuclei in the entire region of light and heavy fragments with mass numbers from 80 to 150, where the moments of inertia are estimated within the hydrodynamic approach. In [18], the moments of inertia were evaluated for the entire working region of fission fragments in the spontaneous fission of the nucleus ^{252}Cf . The study found that, for the entire specified region, the hydrodynamic model is most applicable because of strong

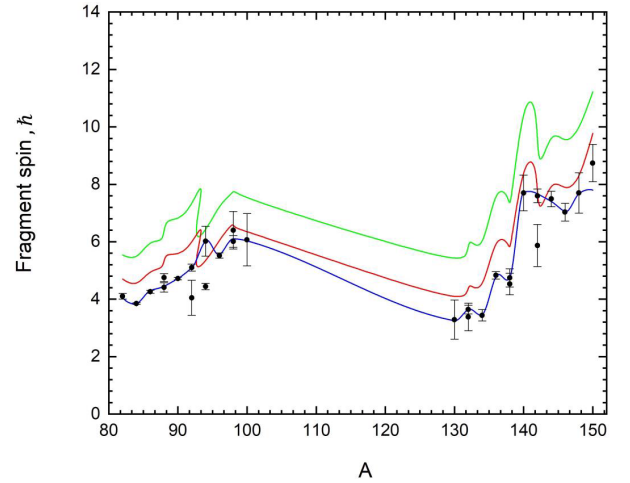


Fig. 5. (color online) Dependence of the mean spin on the mass of forced threshold fission fragments of ^{232}Th , obtained using three different estimates of the moments of inertia. The green line corresponds to the superfluid approach with an oscillatory potential, the red line to the rectangular potential, and the blue line to the hydrodynamic model. Experimental data are from [1].

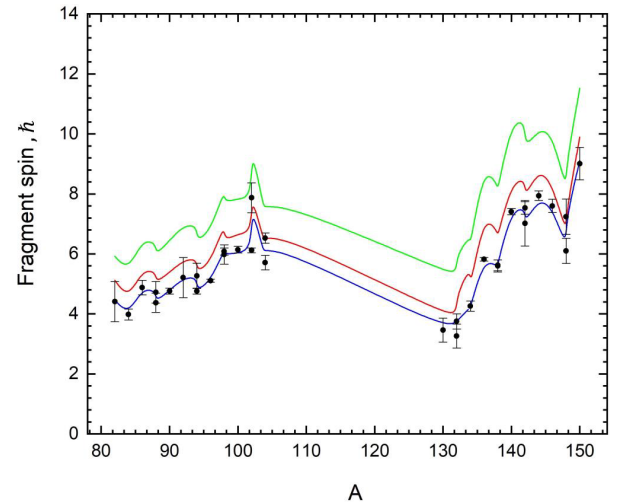


Fig. 6. (color online) Dependence of the mean spin on the mass of forced threshold fission fragments of ^{238}U , calculated using three different estimates of the moments of inertia. The green line corresponds to the superfluid approach with an oscillatory potential, the red line to the rectangular potential, and the blue line to the hydrodynamic model. Experimental data are from [1].

nonequilibrium quadrupole deformations significantly exceeding the equilibrium values. In such cases, the nucleon spacings become smaller than the nucleus size, leading to the predominance of collective effects. In the context of threshold fission of the considered nuclei $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$, a similar relation between equilibrium and nonequilibrium deformation is preserved as observed in the entire region. Therefore, as in the case of

spontaneous fission, the most accurate agreement is achieved using the hydrodynamic model. An additional factor contributing to this agreement was the consideration of neck dynamics between fragments. These results highlight the need for a deeper theory that can integrate the mechanisms of formation of moments of inertia as well as vibrational frequencies and fragment spins, addressing broader aspects of nuclear fission. Given these difficulties, the choice to focus on the forced threshold fission of $^{232}\text{Th}(n, f)$ and $^{238}\text{U}(n, f)$ nuclei is justified by the need to utilize the most complete and reliable experimental data. The next section details why these particular isotopes were chosen and discusses the limitations of data availability for the other nuclei.

III. DISCUSSION

The study was originally planned within a broader context, encompassing a range of actinide isotopes undergoing forced fission by threshold and thermal energy neutrons, such as ^{232}Th , $^{238-242}\text{Pu}$, and $^{233-238}\text{U}$, to perform a comprehensive comparative analysis of the fission mechanism of these nuclei. However, the study faced significant limitations owing to the scarcity of experimental data. To perform calculations based on the proposed methodology [15], we require experimental values of the instantaneous neutron multiplicity. This constraint considerably limited the scope of the study, focusing only on isotopes such as ^{232}Th [30], ^{238}U [17], ^{240}Pu [31], ^{235}U , ^{237}Np , and ^{239}Pu [32], for which appropriate experimental data are available.

Additionally, verification and validation of the computational results require similar experimental neutron distributions for other isotopes, which posed a significant obstacle. The lack of such data for several other actinide nuclei has significantly restricted the possibility of conducting comprehensive model verification and broader comparative analysis.

Another important aspect is the availability of data on SDs for the aforementioned actinide nuclei. In addition to the results discussed earlier for the nuclei ^{232}Th and ^{238}U , described in [1], similar experimental SD data for heavy fission fragments were found in [31]. However, these data raise significant doubts. The main problem is that the values of spins in this study appear to be overestimated. This is clearly demonstrated in Figs. 7 and 8, where a visual comparison is presented. A particularly noticeable overestimation of spin values is observed in the interval of mass numbers $128 \leq A_f \leq 140$, which attracts attention because this region is close to magic nuclei. Moreover, this is particularly pronounced for even-even nuclei in this region, whereas for even-odd nuclei, the deviations are less significant. This discrepancy is evident since the fragments in this region should have small moments of inertia, according to Tables I ($^{232}\text{Th}(n, f)$)

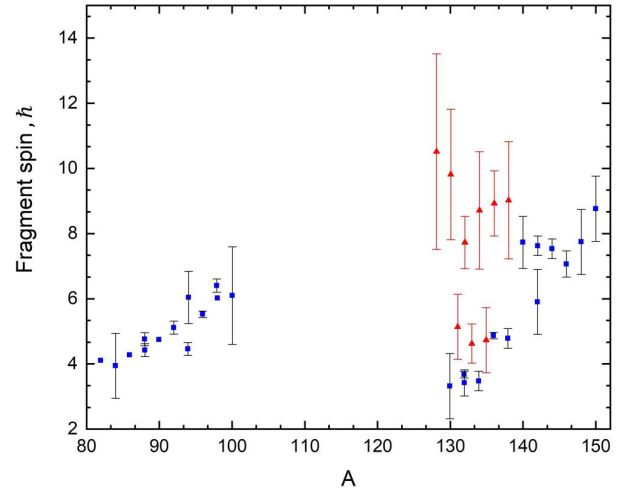


Fig. 7. (color online) Comparison of experimental average spin values as a function of the mass of forced fission fragments of $^{232}\text{Th}(n, f)$. Red triangles indicate results from [31], and blue squares indicate those from [1].

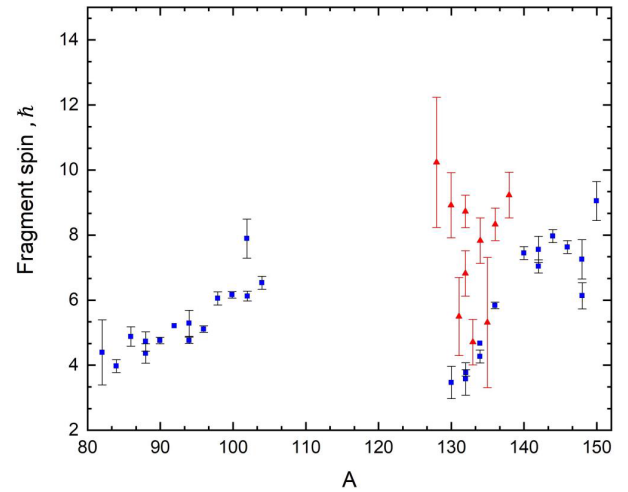


Fig. 8. (color online) Comparison of experimental average spin values as a function of the mass of stimulated fission fragments of $^{238}\text{U}(n, f)$. Red triangles indicate results from [31], and blue squares indicate those from [1].

and II ($^{238}\text{U}(n, f)$), which determine the formation of spins, as correctly noted in [2, 3]. The observed discrepancy for both nuclei underscores the importance of using only modern data on the SD of fission fragments for a correct comparison.

Regarding the isotopes ^{237}Np , ^{233}U , ^{234}U , ^{235}U , ^{238}Pu , ^{239}Pu , ^{240}Pu , ^{241}Pu , and ^{242}Pu , modern SD data for these isotopes are not currently available, although similar data are present in earlier studies [31]. Because the results presented in these works cannot be confirmed using modern experiments such as [1], only up-to-date experimental data have been used to validate the models in this study. Thus, the lack of up-to-date and reliable SD data for other isotopes, including ^{237}Np , ^{233}U , ^{234}U , ^{235}U ,

^{238}Pu , ^{239}Pu , ^{240}Pu , ^{241}Pu , and ^{242}Pu , limited the scope of our study, which focused on the forced threshold fission of nuclei ^{232}Th and ^{238}U , for which the most reliable experimental data are available.

IV. CONCLUSION

This study extends methodological approaches originally developed for the spontaneous fission of ^{252}Cf [18] to the neutron-induced threshold fission of ^{232}Th and ^{238}U nuclei. A comprehensive investigation of fission fragment moment of inertia behavior has been conducted, enabling the identification of characteristic features inherent to different theoretical models employed for their description. The performed analysis yields several fundamental conclusions bearing significant implications for fission theory development.

The developed indirect methodology, based on comparative analysis of fragment mean spin values, demonstrates the inadequacy of superfluid models employing both oscillator and rectangular potentials under conditions of substantial non-equilibrium deformations. Our analysis unequivocally establishes that achieving consistent agreement between theoretical predictions and experimental data [1] for both nuclei across the complete mass range of light and heavy fragments ($A = 80\text{--}150$) necessitates implementation of the hydrodynamic approach for moment of inertia estimation.

These findings are consistent with conclusions from previous comprehensive research on fragment moments of inertia in spontaneous fission [18], which established hydrodynamic model dominance throughout the mass number range. For threshold fission of ^{232}Th and ^{238}U nuclei, an analogous relationship between equilibrium and non-equilibrium deformation parameters persists across the entire investigated mass region. Consequently, optimal theory-experiment correspondence is achieved through hydrodynamic moment of inertia model implementation, mirroring results obtained for spontaneous fission.

Under conditions of small quadrupole deformations approaching equilibrium values, an adequate description is provided by Cooper pairing and superfluid nucleon-nucleon correlations. The superfluid nuclear model with oscillator potential yields satisfactory results in these regimes. However, upon fragment transition to non-equilibrium deformation domains (reaching anomalously high values approaching unity), where the mean free path becomes smaller than nuclear dimensions, the dominant description is provided by the hydrodynamic model with the potential character of collective nucleon motion. These conclusions are confirmed through a detailed analysis of Figs. 5–6 and Tables 1–2.

Consequently, the research findings demonstrate the

necessity of employing distinct theoretical frameworks contingent upon the nuclear deformation magnitude. The obtained conclusions hold considerable significance for both the broad nuclear physics community and computational software developers, particularly authors of the FREYA code implementing "at hot" moment of inertia approximations for spin distribution calculations. This investigation establishes the superiority of the presented approaches over conventional approximations, thereby providing foundations for substantial refinement of existing computational methodologies.

The singular importance of these results lies in conducting the first comprehensive comparative analysis of nuclear moment of inertia models utilizing diverse theoretical frameworks, yielding novel insights into their formation mechanisms. Further investigations examining model applicability across broader nuclear ranges are required to broaden our understanding of nuclear fission. Such endeavors will not only refine respective domains of model adequacy but also expand the frontiers of contemporary quantum fission theory.

A logical next step would be to apply this methodology to nuclei undergoing thermal neutron fission, which are crucial for reactor energy production—specifically isotopes ^{233}U , ^{235}U , ^{239}Pu , and ^{241}Pu . However, meticulous analysis has revealed significant discrepancies between late 20th-century compound fission system spin distributions and contemporary experimental data. Early studies of these isotopes [^{237}Np , ^{233}U , ^{234}U , ^{235}U , ^{238}Pu , ^{239}Pu , ^{240}Pu , ^{241}Pu , and ^{242}Pu] exhibit systematic overestimation of spin values, raising serious concerns regarding their reliability. The contradiction between elevated spin values for fission fragments of near-magic actinide nuclei and modern theoretical frameworks [1] necessitated an investigation on transition toward higher energy regimes, specifically the threshold fission of ^{232}Th and ^{238}U induced by 2 MeV neutrons.

Contemporary experimental data [1] for ^{232}Th and ^{238}U nuclei demonstrate excellent agreement with current theoretical models. Because these systems represent highly excited compound nuclei, this agreement indirectly validates our methodological approach for less-excited systems. Nevertheless, definitive verification requires additional experimental investigations, potentially utilizing apparatus previously employed by the Wilson group for spontaneous ^{252}Cf fission and threshold fission studies of ^{232}Th and ^{238}U [1].

In summary, this research provides significant contributions to understanding fission fragment internal structure and moment of inertia formation mechanisms, thereby creating new avenues for investigating nuclear reactions and their applications across diverse technological and scientific domains.

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